



Short Communication

Economic and Performance Analysis of Thermal System

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Available online at: www.isca.in

(Received 11th February 2012, revised 16th February 2012, accepted 23rd February 2012)

Abstract

For the feasibility of any thermal system economic analysis is must. In the present work economic analysis of a cogeneration power plant is made for increasing the efficiency of cycle. From the literature it is being observe that for increased efficiency the factor which should be taken in to consideration are: air compressor efficiency, gas turbine efficiency, mass flow rate of air, turbine inlet temperature, pressure loss and size of combustion chamber, LMTD for heat transfer surfaces, cycle pressure ratio and mass of steam to be produced. Mathematical model available in literature is used and a computer program in software MATLAB is executed for the analysis. Trend observed for the increase in cost are tabulated in the results.

Keywords: GTCC, HRSG, LMTD

Introduction

The economy of India, a developing country, has grown rapidly in recent years, along with the electrical demand. In recent years, the use of gas turbine for power generation has increased dramatically worldwide. According to world energy forecasts, fossil fuels like coal, oil, and natural gas will continue to be the main energy sources for power generation in the near future in India as well as worldwide. Large-scale natural gas production in India with improved gas turbine technology has made combined cycle power plants a viable option. The thermal efficiency of gas turbine combined cycle (GTCC) power plants can reach 60% that is far more than that of conventional coal-fired steam turbine plants, which not only conserves our limited reserves but also reduces emissions and protects our lives and environment^{1,2,3}. Larger gas turbines with higher power outputs are mainly used in combined cycle plants for heat and power cogeneration^{4,5,6,7,8,9}. The main financial and cash flow concepts are as follows:

Initial equity: The portion of the total investment is paid by the owner's funds. The remainder is paid with borrowed money.

Years for payback of equity: The time required to recoup the initial equity put up by the plant owners from the net plant cash flow.

Net cash flow: The net amount of cash generated per year.

Cumulative net cash flow: The sum of annual net cash flows for the plant over its lifetime.

Operating income = Total revenues – total operating expenses.

Total revenues include electricity and steam revenues. In the present work purchase equipment cost of air compressor, combustion chamber, gas turbine, air preheater and heat recovery steam generator (HRSG) is calculated on the basis of different operating parameters.

Material and Methods

The following cost functions for compressor, combustor, turbine, air preheater and HRSG are used for the analysis:

$$Compressor = \frac{71.10 \times m_{air}}{0.9 - \eta_{is}} r_c \times \ln(r_c)$$

$$Combustor = \frac{46.08 \times m_{air}}{0.995 - \% \Delta P_{cc}} \times [1 + \exp(0.018T_{max} - 26.4)]$$

$$Turbine = \frac{479.34 \times m_{gas}}{0.92 - \eta_{is}} \cdot \ln r_t \times [1 + \exp(0.036T_{max} - 54.4)]$$

$$AirPreheater = 4122 \left(\frac{m_g (h_{in} - h_{out})}{18 \cdot \Delta T_{LMTDAph}} \right)^{0.6}$$

$$HRSG = 6570 \left[\left(\frac{Q_{ec}}{\Delta T_{LMTDec}} \right)^{0.8} + \left(\frac{Q_{ev}}{\Delta T_{LMTDev}} \right)^{0.8} \right] + 21276 \cdot m_{st} + 1184.4 m_g^{1.2}$$

The scheme outlined above has been numerically studied using a code developed in MATLAB.

Results and Discussion

With the increase of GT cycle output, the GTCC output increases even more, so the difference of GT and GTCC outputs increases. Therefore, larger gas turbines in combined cycle

power plants will experience a greater output increase than smaller gas turbines, since the electrical efficiency of the combined cycle is higher than that of a simple cycle. The efficiencies of the smaller gas turbines are not directly related to size as with the medium and large turbines where the electrical efficiency of both the GT and GTCC increases slowly with increasing output. Therefore, large gas turbines with their higher electrical efficiencies in both simple and combined cycle systems will provide better energy conservation and utilization.

The total investment includes the cost of specialized equipment, plant site infrastructure, mechanical infrastructure, buildings, etc. The specialized equipment includes the gas turbine, the steam turbine, the heat recovery boiler, the water-cooled condenser, the fuel gas compressor, the continuous emissions monitoring system, the distributed control system, and the transmission and generating voltage equipment packages. Here purchase equipment cost of air compressor, combustion chamber, gas turbine, air preheater and heat recovery steam generator (HRSG) is calculated on the basis of different operating parameters. Cost of HRSG depends upon the Log

mean temperature difference (LMTD), mass of steam produced and mass of flue gases passing through it.

With increase in LMTD cost of HRSG comes down but with increase in mass of steam and flue gases cost of HRSG increases. Cost of air preheater depends upon LMTD and mass of flue gases and same trend that of HRSG is observed in it. Cost of air compressor is dependent upon the mass of air entering the compressor, compression ratio and compressor efficiency. As the value of all these three parameters increases, cost of air compressor also increases. Cost of combustion chamber (CC) depends upon the mass of air entering the combustion chamber, pressure losses in combustion chamber and combustion chamber outlet temperature. As CC outlet temperature increases, cost of material also increases. Secondly for higher mass flow rate in CC, size of CC should be large. Both these factors increase the cost of combustion chamber. For higher turbine inlet temperature (TIT), turbine blade material becomes costly. For higher mass flow rate of air, larger gas turbine is required. Same trend is observed for the case higher efficiency and higher turbine pressure ratio. However, other factors must also be taken into consideration.

Table-1
Purchase equipment cost (PEC) of HRSG

| LMTD | 100 | 115 | 130 | 145 | 160 |
|---------------------------|-----------|-----------|-----------|-----------|-----------|
| PEC of HRSG | 426957023 | 426856699 | 426772596 | 426708276 | 426655499 |
| Mass of steam (Kg/s) | 20000 | 25000 | 30000 | 35000 | 40000 |
| PEC of HRSG | 426957023 | 958629405 | 106500940 | 117138940 | 127776940 |
| Mass of flue gases (Kg/s) | 80 | 85 | 90 | 95 | 100 |
| PEC of HRSG | 426957023 | 426974197 | 426991579 | 427009153 | 427026913 |

Table-2
Purchase equipment cost of air preheater

| LMTD | 100 | 110 | 120 | 130 | 140 | 150 |
|---------------------------|--------|--------|--------|--------|--------|--------|
| PEC air preheater | 151236 | 142827 | 135563 | 129207 | 123587 | 475826 |
| Mass of flue gases (Kg/s) | 80 | 85 | 90 | 95 | 100 | 105 |
| PEC air preheater | 151235 | 156765 | 162234 | 167583 | 172821 | 177955 |

Table-3
Purchase equipment cost of air compressor

| Mass of air (Kg/s) | 80 | 85 | 90 | 95 | 100 |
|-----------------------|--------|---------|---------|---------|---------|
| PEC compressor | 946483 | 1005638 | 1064793 | 1123948 | 1183104 |
| Compression Ratio | 8 | 10 | 12 | 14 | 16 |
| PEC compressor | 946483 | 1308240 | 1692748 | 2102284 | 2520921 |
| Compressor Efficiency | 0.8 | 0.82 | 0.84 | 0.86 | 0.88 |
| PEC compressor | 946483 | 1183104 | 1577472 | 2366208 | 4732416 |

Table-4
Purchase equipment cost of combustion chamber

| Mass of air (Kg/s) | 80 | 85 | 90 | 95 | 100 | 105 |
|-----------------------|--------|--------|--------|--------|--------|--------|
| PEC of CC | 111756 | 118740 | 125725 | 132710 | 139695 | 146679 |
| Pressure loss in CC | 0.10 | 0.09 | 0.08 | 0.07 | 0.06 | 0.05 |
| PEC of CC | 111756 | 124903 | 141557 | 163335 | 193033 | 235929 |
| CC outlet temperature | 1373 | 1423 | 1473 | 1523 | 1573 | 1623 |
| PEC CC | 45788 | 56266 | 82264 | 146679 | 301896 | 686058 |

Table-5
Purchase equipment cost of gas turbine

| Mass of flue gases | 80 | 85 | 90 | 95 | 100 | 105 |
|------------------------|--------|--------|---------|---------|---------|----------|
| PEC gas turbine | 669271 | 711100 | 752930 | 794625 | 836448 | 878270 |
| TIT | 1373 | 1423 | 1473 | 1523 | 1573 | 1623 |
| PEC gas turbine | 669271 | 692601 | 833514 | 1681652 | 6832959 | 37321055 |
| Turbine pressure ratio | 8 | 10 | 12 | 14 | 16 | 18 |
| PEC gas turbine | 669271 | 740059 | 799585 | 849156 | 892121 | 930020 |
| GT Efficiency | 0.8 | 0.82 | 0.84 | 0.86 | 0.88 | 0.9 |
| PEC gas turbine | 669271 | 803125 | 1003906 | 1338542 | 2007813 | 4015626 |

The increase in the annual fuel consumption is almost proportional to the GTCC output. Then, the maximum fuel consumption and the maximum output are both from the largest system. Larger gas turbines will be better choices for Indian GTCC power plants due to their higher electrical efficiencies, shorter payback time, and lower owner's cost per MW, but their total investment cost and annual fuel needs are very high. India, therefore, needs to select suitable sized gas turbines according to the specific economic conditions.

References

1. Saravanamuttoo H.I.H., Rogers G.F.C. and Cohen H., Gas Turbine Theory, *Pearson Education Limited*, 1-20 (2001)
2. De Biasi V., M701G2 combined cycle is rated at 489 MW and 58.7% efficiency, *Gas Turbine World*, 7, 9-13 (2000)
3. Xiaotao Z., Hideaki S., Weidou N. and Zheng L., Economics and Performance Forecast of Gas Turbine Combined Cycle, *Tsinghua Science and Technology*, 10(5), 633-636 (2005)
4. Masada J. and Fukue I., Operating experience in refinery application of the 13 MW-class heavy duty MF-111 gas turbine engine, *Gas Turbine and Aeroengine Congress and Exposition*, Brussels, Belgium, (1990)
5. Tsukuda Y., Akita E., Arimura H., Tomita Y. and Kuwabara M., The operating experience of the next generation M501G/M701G gas turbine, *Proceedings of ASME TURBO EXPO 2001*, New Orleans, Louisiana (2001)
6. Swanekamp R., Gas turbines, combined-cycles harvest record orders, *Power*, 3, 30-32 (2000)
7. Sato M., Kobayashi Y., Matsuzaki H., Aoki S., Tsukuda Y. and Akita E., Final report of the key technology development program for a next generation high-temperature gas turbine, *Journal of Engineering for Gas Turbine and Power*, 119, 617-623 (1997)
8. Dev N., Samsher and Kachhwaha S.S., Computational Analysis of Dual Pressure Non-reheat Combined-Cycle Power Plant with Change in Drum Pressures, *International Journal of Applied Engineering Research*, 5(8), 1307-1313 (2010)
9. Valero A., Lozano M.A., Serra L., Tsatsaronis G, Pisa J., Frangopoulos C. and Von Spakovsky M.R., CGAM Problem: Definition and Conventional Solution, *Energy*, 19(3), 279-286 (1994)